

## Basic measures of stress

### Stress Tensor

$$\mathbf{T} = \begin{pmatrix} \sigma_{11} & \sigma_{12} & \sigma_{13} \\ \sigma_{21} & \sigma_{22} & \sigma_{23} \\ \sigma_{31} & \sigma_{32} & \sigma_{33} \end{pmatrix}$$

where  $\sigma_{12}$  is shear stress acting parallel to axis 2 on the plane perpendicular to axis 1

$\mathbf{T}$  is symmetric (i.e.  $\sigma_{xy} = \sigma_{yx}$ )

### Principal stresses

$\sigma_1 > \sigma_2 > \sigma_3$  are the normal stresses that operate parallel to the eigenvectors of  $\mathbf{T}$  (the stress axes). If the stress axes coincide with the coordinate axes then

$$\mathbf{T} = \begin{pmatrix} \sigma_1 & 0 & 0 \\ 0 & \sigma_2 & 0 \\ 0 & 0 & \sigma_3 \end{pmatrix}$$

### Mean stress

If the magnitudes of the principal stresses are  $\sigma_1$   $\sigma_2$   $\sigma_3$  then:

$$\text{mean stress } \sigma_m = (\sigma_1 + \sigma_2 + \sigma_3)/3$$

### Differential stress

Differential stress  $\sigma_d = \sigma_1 - \sigma_3$

Maximum shear stress =  $\sigma_d/2$

### Deviatoric stress

$$\mathbf{T}_d = \begin{pmatrix} \sigma_{11} - \sigma_m & \sigma_{12} & \sigma_{13} \\ \sigma_{21} & \sigma_{22} - \sigma_m & \sigma_{23} \\ \sigma_{31} & \sigma_{32} & \sigma_{33} - \sigma_m \end{pmatrix}$$

### Stress on a plane

For a plane with unit normal vector vector  $\mathbf{x}$ ,

$$\boldsymbol{\sigma} = \mathbf{T} \cdot \mathbf{x}$$

Resolved normal stress  $\sigma_n = \boldsymbol{\sigma} \cdot \mathbf{x}$

Resolved shear stress  $\sigma_s^2 = \sqrt{(\sigma^2 - \sigma_n^2)}$

Where  $\sigma$ ,  $\sigma_n$ ,  $\sigma_s$  are the magnitudes of the resolved shear stress, and its normal and shear components.

### Effective stress

$$\text{Effective stress} = \begin{pmatrix} \sigma_{11} - P_f & \sigma_{12} & \sigma_{13} \\ \sigma_{21} & \sigma_{22} - P_f & \sigma_{23} \\ \sigma_{31} & \sigma_{32} & \sigma_{33} - P_f \end{pmatrix}$$

where  $P_f$  = pore fluid pressure

## Stress states

If  $\rho$  is the average density of overlying material,  $g$  is the acceleration due to gravity, and  $z$  is depth, and  $\nu$  is Poisson's ratio

### Lithostatic/hydrostatic stress

$$\sigma_1 = \sigma_2 = \sigma_3 = \rho g z$$

### Uniaxial-strain reference state

$$\sigma_x = \sigma_y = \frac{\nu}{1-\nu} \sigma_z = \frac{\nu}{1-\nu} \rho g z$$

## Stress-strain relationships

(Elastic/brittle behaviour)

### Elastic strain

Linear stress  $\sigma_n = E \cdot e$

Poisson's ratio  $\nu = -e_1/e_3$

shear stress  $\sigma_s = G \cdot \gamma$

mean stress  $\sigma_m = -K \Delta$

where  $E$  = Young's modulus of elasticity;

$G$  = shear modulus of elasticity;

$K$  = bulk modulus of elasticity;

$e_1$ ,  $e_3$  are principal extensions of sample under uniaxial compression.

Relationships between the elastic moduli

$$G = \frac{E}{2(1+\nu)} \quad K = \frac{E}{3(1-2\nu)}$$

### Brittle Failure

Coulomb fracture criterion

$$\sigma_s = C + \sigma_n \tan \phi$$

where  $C$  is a constant and  $\phi$  is the angle of internal friction.

Angle between pole to failure plane and  $\sigma_1$

$$\theta = 45^\circ + \phi/2$$

### "Byerlee's law" for movement on existing fractures

$$\sigma_s = 0.85 \sigma_n \quad (\sigma_n < 200 \text{ MPa})$$

$$\sigma_s = 50 \text{ MPa} + 0.60 \sigma_n \quad (\sigma_n > 200 \text{ MPa})$$